

Note: State your assumption clearly if required & start a fresh page for answering each question

1. The exothermic reaction $A \rightarrow B + C$ was carried out adiabatically and the following data recorded. The entering molar flowrate of A was 300 mol/min. [15 M]
- What are the PFR and CSTR volumes necessary to achieve 40% conversion?
 - What is the maximum conversion that can be achieved in a 105-dm³ CSTR?
 - What conversion can be achieved if a 72-dm³ PFR is followed in series by a 24-dm³ CSTR?
 - What conversion can be achieved if a 24 dm³ CSTR is followed in a series by a 72-dm³ PFR?

X	0	0.2	0.4	0.45	0.5	0.6	0.8	0.9
$-r_A$ (mol/dm ³ ·min)	1.0	1.67	5.0	5.0	5.0	5.0	1.25	0.91

2. The first-order reversible liquid reaction $A \rightleftharpoons R$, $C_{A0} = 0.5$ mol/ lit, $C_{R0} = 0$, takes place in a batch reactor. After 8 minutes, conversion of A is 33.3% while equilibrium conversion is 66.7%. Find the rate equation for this reaction. [8 M]
3. Find the first-order rate constant for the disappearance of A in the gas reaction $2A \rightarrow R$ if, on holding the pressure constant, the volume of the reaction mixture, starting with 80% A, decreases by 20% in 3 min. [7 M]
4. The homogeneous gas decomposition of phosphine $4 PH_3(g) \rightarrow P_4(g) + 6H_2(g)$ proceeds at 649 °C with the first-order rate $-r_{PH_3} = (10/hr)C_{PH_3}$. What size of plug flow reactor operating at 649 °C and 460 kPa can produce 80% conversion of a feed consisting of 40 mol of phosphine and 20 mol of argon per hour? [15 M]
5. The first order homogeneous gas phase reaction $A \rightarrow 2.5 R$ is carried out in an isothermal batch reactor at 2 atm pressure with 80 mole % A and 20 mole % inerts, and the volume increased by 60% in 20 minutes. In the case of a constant-volume reactor, determine the time required (for the same reaction) for the pressure to rise to 8 atm if the initial pressure is 5 atm, 2 atm of which consists of inerts. (i.e., the contribution of inerts present is 2 atm to the initial total pressure of 5 atm) [20 M]
6. Our company has a continuous stirred fermentation process (second order irreversible, constant hold-up) in an open tank where the liquid is kept at a constant height. The tank has a catwalk around it so the sediment can be removed. The process has been run for many years by a loyal employee who is a bit overweight and has been rumored to have a drinking habit. Yesterday, he was missing for the first time in many years. The tank has a volume of 1000 liters. The data log shows that the conversion from the process decreased from its normal 75% to 72%, but the flow rate did not change. (Assume the substances in the tank, and the person have the same density- equal to 1.0 kg/ lit)
- How overweight was he?
 - If you were the design engineer for this process, you could be in considerable trouble. How should you have modified the process to avoid such accidents? [10 M]

7. The liquid-phase reaction was carried out in a CSTR. For an entering concentration of 2 mol/dm³. the conversion was 40%. For the same reactor volume and entering conditions as the CSTR, the expected PFR conversion is 48.6%. However, the PFR conversion was amazingly 50% exactly. Brainstorm reasons for the disparity. Quantitatively show how these conversions came about (i.e., the expected and actual conversions). [15 M]

ALL THE BEST

The following may or may not be required to solve the above problems

$$\Rightarrow \frac{1}{C_A} - \frac{1}{C_{A0}} = kt$$

$$\frac{1}{C_A} - \frac{1}{C_{A0}} = \frac{1}{C_{A0}} \frac{X_A}{1 - X_A} = 2kt, \quad M = 2$$

$$\ln \frac{C_{A0}(C_0 - C_A)}{C_A(C_0 - C_{A0})} = \ln \frac{C_R/C_{R0}}{C_A/C_{A0}} = C_0 kt = (C_{A0} + C_{R0}) kt$$

$$\ln \frac{M + X_A}{M(1 - X_A)} = C_{A0}(M + 1)kt = (C_{A0} + C_{R0})kt$$

$$\frac{\ln(C_{A0}/C_A)}{C_{A0} - C_A} = -k_2 + \frac{k_1 t}{C_{A0} - C_A}$$

$$\ln \frac{X_{Ae} - (2X_{Ae} - 1)X_A}{X_{Ae} - X_A} = 2k_1 \left(\frac{1}{X_{Ae}} - 1 \right) C_{A0} t$$

$$\frac{(1 + \varepsilon_A)\Delta V}{V_0 \varepsilon_A - \Delta V} + \varepsilon_A \ln \left(1 - \frac{\Delta V}{\varepsilon_A V_0} \right) = k C_{A0} t$$