## BIRLA INSTITUTE OF TECHNOLOGY AND SCIENCE, PILANI -PILANI CAMPUS

## II Semester 2016-2017

## **CHE F 419: Chemical Process Technology**

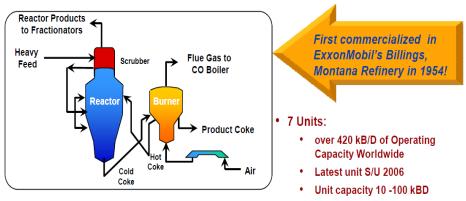
Misemester Examination: 11/03/2017: Closed Book: SET B

טנ	Duration: 1 nour 30 minutes	MM: 15+50+25= 90			
	Name: ID	No.			
	Marks obtained = + =				
	. Paper is completely CLOSED BOOK:BLANKS+ Q/A of TOTAl = 9	 D marks			
	. Blanks are to be attempted in the given portion only.				
	. Q 1-3 is to be attempted in question paper itself.				
	. Q-4 IS TO BE ATTEMPTED IN SEPARATE ANSWERSHEET.				
	<ul> <li>Restrict the answers appropriately in space provided.</li> <li>Make the suitable assumptions if any.</li> </ul>				
	Most important catalytic processes in the oil refinery, in terms o	of throughout, are fluid catalytic cracking			
	(FCC), hydrotreating, hydrocracking,a				
	Propane deasphalting is based on the o	f hydrocarbons in propane, that is, on the			
	type of molecule.				
		and fed to the riser			
	reactor together with regenerated catalyst in FCC.				
		ounts of C3 and C4 alkenes in FCC units,			
	because these are valuable as for				
	such as ethene and propene as a result of their high	content.			
	Crude oil often contains water,,,	and water-			
	soluble trace metals.				
	Coke-forming tendencies of heavier distillation products (mainly	atmospheric and vacuum residue) can b			
	reduced by removal of "asphaltenic" materials (large aromatic c	ompounds) by means of			
	A good example is the production of coke for	, which in fact is the largest non-fuel			
	end use for petroleum coke.				
).	.  O. Gas leaving the heater in Flexicoking process is cooled by steam.	generation and then passes through a			
	and for the real				
	The Lurgi moving bed gasifier (Figure 5.13), is operated countercurrently; the coal enters the gasifier at				
	the top and is slowly heated and dried (partial pyrolysis) on its way down whilethe				
	product gas as it exits the reactor.	·			
2.	. Updraft gasifiers produce 5 % to 20%	and so are unsuitable for operation			
	of engines.	·			
	. Winkler fluidized bed gasifier is areactor in	which coal particles in the feedare well			
	mixed with coal particles already undergoing gasification.				

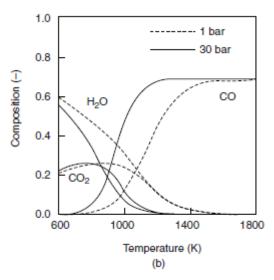
- 1. Answer the following questions
  - a) Why are so many stripper combinations required after main fractionator in modern crude distillation unit? [3]

b) Expalin one important difference between updraft and down draft biomass gasification technologies . [4]

c) How is the direction of outlet streams explained for the reactor & heater combination in the flexicoing process?



d) Given below is the plot shoing the effect of temperature and pressure on equilibrium gas composition in autothermal gasification of coal. How does one explain this obtained trend? [5]



e) How does one explain the data sets given below for the catalytic reforming process (semi, fully & continuous regenerative processes) for naptha? Explain for two parameters only: feed & pressure.

[5]

Table 3.9 Operating conditions in catalytic reforming.

	Semi	Fully	Continuous
Feed H <sub>2</sub> /HC (mol/mol)	10	4-8	4-8
Pressure (bar)	15-35	7-15	3-4
Temperature (K) Catalyst life	740-780 0.5 - 1.5 y	740–780 days – weeks	770–800 days – weeks

2. Alkane dehydrogenation is highly endothermic and high temperatures are required. Furthermore, the thermodynamic equilibrium limits the conversion per pass. Several catalytic dehydrogenation processes are commercially available. These processes differ in the type of catalyst used, the reactor design, the method of heat supply, and the method used for catalyst regeneration. Given the data sheet for all the four technologies in this area, how does one explain the conversion and selectivity for dehydrogenation process for propane & isobutane? How is the trade off established in any two chosen process for the production of desired alkenes? [10+5=15]

 Table 4.5
 Performance of propane and isobutane dehydrogenation processes [17, 19, 21, 22].

Process	Oleflex	Catofin	STARa	FBD
Reactor	adiabatic moving beds	parallel adiabatic fixed beds with swing reactor	isothermal tubular reactors in furnace	fluidized bed
Catalyst	Pt/Al <sub>2</sub> O <sub>3</sub>	Cr/Al <sub>2</sub> O <sub>3</sub>	Pt-Sn/Zn-Al <sub>2</sub> O <sub>3</sub>	Cr/Al <sub>2</sub> O <sub>3</sub>
Catalyst life (y)	1–3	1–2	1–2	not available
Temperature (K)	820-890	860-920	750-890	820-870
Pressure (bar)	1–3	0.1-0.7	3–8	1.1-1.5
Conversion (%)b	P: 25	P: 48-65	P: 30-40	P: 40
	IB: 35	IB: 60-65	IB: 40-55	IB: 50
Selectivity (%)b	P: 89-91	P: 82-87	P: 80-90	P: 89
	IB: 91-93	IB: 93	IB: 92-98	IB: 91

 $<sup>^</sup>a$ Without oxydehydrogenation reactor.

<sup>&</sup>lt;sup>b</sup>P: propane dehydrogenation; IB: isobutane dehydrogenation.

3.	Hydrotreating is essential as a pretreatment step for catalytic reforming of naphtha. The sulfur content of
	the feed to the reforming unit should not exceed 1 ppm. In simple naphtha hydrotreating, the feed in
	evaporated and led through a fixed bed reactor. Draw a complete flowsheet of hydrotreatig plant of heav
	oil showing all the iputs & output streams, taking care of heat integration and separation system used i
	such plants developments. [15]

## 4. THIS IS TO BE ATTEMPTED IN SEPARATE ANSWERSHEET & MAKE A SUITABLE ASSUMPTION IS ANY.

2.7 billion lb/stream day of ethylene is produced using commercial grade ethane as feedstock using steam reformer. Ethane arrives in liquid state at 700 psig and 80° F: Reactants & Product specs.

[25]

- a. Show what all steps would be needed to complete the design of steam cracker.
- b. Carry out the complete material balance for the given process..
- c. Draw the schematic of steam cracker showing all the inputs & outputs from the cracker.

			SN	Component	Mole %	
SNO	Component	Mole %	0	Component	ividic 70	
1.	CH <sub>4</sub>	3	1.	CH <sub>4</sub>	0.6	
2.	$C_2H_6$	94	2.	$C_2H_6$	0.4	
3.	C <sub>3</sub> H <sub>8</sub>	3	3.	$C_2H_4$	99	
4.	CO <sub>2</sub> 800 ppm S Very less in	800 ppm	4.	$C_2H_2$	<10 ppm	
5.		Very less in	5.	H <sub>2</sub> S	<5 ppm	
		ppm	6.	CO <sub>2</sub>	<100 ppm	

The first-order rate constant for ethane is obtained from Table 10.4, p. 446<sup>1</sup>.

$$k_c = 4.717 \times 10^{14} e^{-72.240/R'T}, \text{ sec}^{-1}$$
 (CS-2.1)

where  $T = {}^{\circ}K$  or

$$k_p = \frac{k_c}{RT} = \frac{4.717 \times 10^{14}}{RT} e^{-130.032/RT}, \frac{\text{lb mole}}{(\text{atm})(\text{ft}^3)(\text{sec})}$$
 (CS-2.2)

where  $T = {}^{\circ}\mathbf{R}$  and  $\mathbf{R} = 0.73$ .

			<b>A</b>	E, kcal/g mole
Initiation	$C_2H_6 \rightarrow 2CH_3$ .	(1)	$1.0 \times 10^{16}$	86
	$(CH_3 + C_2H_6 \rightarrow CH_4 + C_2H_5)$	(2)	$3.16 \times 10^{8}$	10.8
Propagation	$\left\{ C_2H_5 \rightarrow C_2H_4 + H \right\}$	(3)	$3.98 \times 10^{13}$	38
	$\begin{cases} CH_3 + C_2H_6 \to CH_4 + C_2H_5 \\ C_2H_5 \to C_2H_4 + H \\ H \cdot + C_2H_6 \to H_2 + C_2H_5 \end{cases}$	(4)	$1.25 \times 10^{11}$	9.7
Termination	$\begin{cases} C_2H_5 \cdot + C_2H_5 \cdot \to n - C_4H_{10} \\ C_2H_5 \cdot + C_2H_5 \cdot \to C_2H_6 + C_2H_4 \end{cases}$	(5a) (5b)	$2.511 \times 10^{10}$	0
Propylene				
formation	$C_2H_5 + C_2H_4 \rightarrow C_3H_6 + CH_3$	(6)	$3.16 \times 10^{9}$	19
Inhibition	$\begin{bmatrix} C_{2}H_{5}^{\cdot} + C_{2}H_{4} \rightleftarrows 1\text{-}C_{4}H_{9}^{\cdot} \\ 1\text{-}C_{4}H_{9}^{\cdot} \to 2\text{-}C_{4}H_{9}^{\cdot} \\ 2\text{-}C_{4}H_{9}^{\cdot} \to C_{3}H_{6} + CH_{3}^{\cdot} \end{bmatrix}$ $H^{\cdot} + C_{2}H_{4} \to C_{2}H_{5}^{\cdot}$	(7)	$5.0118 \times 10^{10}$ Units for $\mathbf{A} = \mathbf{s}$	sec <sup>-1</sup> for Re-
			actions 1 and 3, and 1.( $g$ mole) <sup>-1</sup> sec <sup>-1</sup> for others.	

**Fig. CS-2.1** Free-radical mechanism for ethane cracking. [Reaction 5a can be neglected in terms of product produced and a combined rate constant used,  $k_5 = 1.15k_{5a}(1)$ . Rate equations in terms of partial pressures may be written using RT corrections.]