BIRLA INSTITUTE OF TECHNOLOGY AND SCIENCE, PILANI
First SEMESTER 2023 – 2024
Environmental Sampling and Analytical Methods – Mid semester examination

Course No: EEG501 **Date: 11-10-2023**
Duration: 1.5 hours, 4 PM-5.30 PM **Max. Marks: 30**

Note: All the questions are compulsory. If unit is not mentioned, marks will be deducted. Assume appropriate data if needed.

1. (a) What is the difference between accuracy and precision in environmental analysis? **[2 Marks]**

   (b) Which of the option/options is/are true? Method detection limits are specific to-

   I. Sample matrix
   II. Method
   III. Instrument
   IV. Analytical technique
   V. All of the above **[2 Marks]**

   (c) What is spiking of samples in environmental analysis? **[1 Mark]**

2. (a) The background concentration of Zn in soils of Houston area is normally distributed with a mean of 68 mg/kg and a standard deviation of 5 mg/kg **[3 Marks]**

   i. What percentage of the soil samples will have a concentration <75 mg/kg?
   ii. What percentage of the soil samples will have a concentration >75 mg/kg?
   iii. What percentage of the soil samples will have a concentration between 64 and 75 mg/kg?

   (b) If the same data shown above were obtained from a sample size of n=9 rather than a population (mean=68 mg/kg, standard deviation=5 mg/kg), what are the confidence intervals for two sided confidence levels of 90% and 99%? **[2 Marks]**

3. Studies were conducted to test lead concentrations in surface soils due to atmospheric deposition of emissions from a smelter. Prior information revealed that Pb is higher in the prevailing downwind direction (from East to West). The Pb concentration is also higher in clayed soils than sandy soils. It was determined that a stratified random sampling approach was appropriate. A total of 30 samples were collected, and the number of samples in each stratum was proportionally allocated based on the estimated percentage land area under the specified wind direction. Estimate the overall means and standard deviation.

   Raw data (unit in mg/kg): S1 (Downwind clayed soil) 80, 75, 89, 65, 73, 77, 74, 83, 82, 85, 76, 87, 77, 90, 72; S2 (Downwind sandy soil) 66, 68, 65, 60, 70, 64; S3 (Perpendicular wind clayey soil) 60, 55, 59, 57, 53; S4 (Perpendicular wind sandy soil) 53, 51, 49, 47. Stratum weight of S1 is 0.45, S2 is 0.25, S3 is 0.16, S4 is 0.14. **[5 Marks]**

4. (a) What is grab and composite samplings? **[2 Mark]**
   (b) What are the different equipment that can be used for surface water and wastewater sampling? **[1 Marks]**

5. Determine the amount of magnetite, Fe_3O_4, in an impure ore. 1.64 g of impure sample is dissolved in concentrated HCl, giving a mixture of Fe^{2+} and Fe^{3+}. After adding HNO_3 to oxidize Fe^{2+} to Fe^{3+} and diluting with water, Fe^{3+} is precipitated as $Fe(OH)_3$ by adding NH_3. Filtering, rinsing, and igniting the precipitate provides 0.95 g of pure Fe_2O_3. Calculate the % w/w Fe_3O_4 in the sample. Atomic mass of Fe is 55.8 g. **[5 Marks]**

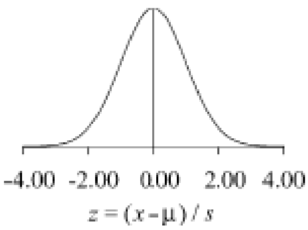
6. 6 g of an unknown material is analyzed for its chloride content. The sample was dissolved in 50 mL of analyte free water and titrated with 18.2 mL of 0.141 N mercuric nitrate, $Hg(NO_3)_2$ standard solution. What is the percentage of w/w chloride content of the material? Atomic mass of Hg is 200.6 g. **[5 Marks]**

7. What will be the pH of the ammonia solution (0.4 M) if k_b for NH_3 is 1.8×10^{-5} **[2 Marks]**

Equations and Tables to solve questions

$\mathrm{CI} = \bar{x} \pm t_{n-1,1-\frac{\alpha}{2}}(\frac{s}{\sqrt{n}})$	$s = \sqrt{\frac{\sum_{i=1}^{n}(x_i - \bar{x})^2}{n-1}}$	$\bar{x} = \sum_{k=1}^{r} w_k \bar{x}_k$	$s^2 = \sum_{k=1}^{r} \frac{w_k^2 s_k^2}{n_k}$

APPENDIX C1. STANDARD NORMAL CUMULATIVE PROBABILITIES



The entries in the table are the areas (probablities) under the standard normal curve from $z = 0$ to $z = z$. 1

z	0	1	2	3	4	5	6	7	8	9
0.0	0.0000	0.0040	0.0080	0.0120	0.0160	0.0199	0.0239	0.0279	0.0319	0.0359
0.1	0.0398	0.0438	0.0478	0.0517	0.0557	0.0596	0.0636	0.0675	0.0714	0.0753
0.2	0.0793	0.0832	0.0871	0.0910	0.0948	0.0987	0.1026	0.1064	0.1103	0.1141
0.3	0.1179	0.1217	0.1255	0.1293	0.1331	0.1368	0.1406	0.1443	0.1480	0.1517
0.4	0.1554	0.1591	0.1628	0.1664	0.1700	0.1736	0.1772	0.1808	0.1844	0.1879
0.5	0.1915	0.1950	0.1985	0.2019	0.2054	0.2088	0.2123	0.2157	0.2190	0.2224
0.6	0.2257	0.2291	0.2324	0.2357	0.2389	0.2422	0.2454	0.2486	0.2517	0.2549
0.7	0.2580	0.2611	0.2642	0.2673	0.2704	0.2734	0.2764	0.2794	0.2823	0.2852
0.8	0.2881	0.2910	0.2939	0.2967	0.2995	0.3023	0.3051	0.3078	0.3106	0.3133
0.9	0.3159	0.3186	0.3212	0.3238	0.3264	0.3289	0.3315	0.3340	0.3365	0.3389
1.0	0.3413	0.3438	0.3461	0.3485	0.3508	0.3531	0.3554	0.3577	0.3599	0.3621
1.1	0.3643	0.3665	0.3686	0.3708	0.3729	0.3749	0.3770	0.3790	0.3810	0.3830
1.2	0.3849	0.3869	0.3888	0.3907	0.3925	0.3944	0.3962	0.3980	0.3997	0.4015
1.3	0.4032	0.4049	0.4066	0.4082	0.4099	0.4115	0.4131	0.4147	0.4162	0.4177
1.4	0.4192	0.4207	0.4222	0.4236	0.4251	0.4265	0.4279	0.4292	0.4306	0.4319
1.5	0.4332	0.4345	0.4357	0.4370	0.4382	0.4394	0.4406	0.4418	0.4429	0.4441
1.6	0.4452	0.4463	0.4474	0.4484	0.4495	0.4505	0.4515	0.4525	0.4535	0.4545
1.7	0.4554	0.4564	0.4573	0.4582	0.4591	0.4599	0.4608	0.4616	0.4625	0.4633
1.8	0.4641	0.4649	0.4656	0.4664	0.4671	0.4678	0.4686	0.4693	0.4699	0.4706
1.9	0.4713	0.4719	0.4726	0.4732	0.4738	0.4744	0.4750	0.4756	0.4761	0.4767
2.0	0.4772	0.4778	0.4783	0.4788	0.4793	0.4798	0.4803	0.4808	0.4812	0.4817
2.1	0.4821	0.4826	0.4830	0.4834	0.4838	0.4842	0.4846	0.4850	0.4854	0.4857
2.2	0.4861	0.4864	0.4868	0.4871	0.4875	0.4878	0.4881	0.4884	0.4887	0.4890
2.3	0.4893	0.4896	0.4898	0.4901	0.4904	0.4906	0.4909	0.4911	0.4913	0.4916
2.4	0.4918	0.4920	0.4922	0.4925	0.4927	0.4929	0.4931	0.4932	0.4934	0.4936
2.5	0.4938	0.4940	0.4941	0.4943	0.4945	0.4946	0.4948	0.4949	0.4951	0.4952
2.6	0.4953	0.4955	0.4956	0.4957	0.4959	0.4960	0.4961	0.4962	0.4963	0.4964
2.7	0.4965	0.4966	0.4967	0.4968	0.4969	0.4970	0.4971	0.4972	0.4973	0.4974
2.8	0.4974	0.4975	0.4976	0.4977	0.4977	0.4978	0.4979	0.4979	0.4980	0.4981
2.9	0.4981	0.4982	0.4982	0.4983	0.4984	0.4984	0.4985	0.4985	0.4986	0.4986
3.0	0.4987	0.4987	0.4987	0.4988	0.4988	0.4989	0.4989	0.4989	0.4990	0.4990
3.1	0.4990	0.4991	0.4991	0.4991	0.4992	0.4992	0.4992	0.4992	0.4993	0.4993
3.2	0.4993	0.4993	0.4994	0.4994	0.4994	0.4994	0.4994	0.4995	0.4995	0.4995
3.3	0.4995	0.4995	0.4995	0.4996	0.4996	0.4996	0.4996	0.4996	0.4996	0.4997
3.4	0.4997	0.4997	0.4997	0.4997	0.4997	0.4997	0.4997	0.4997	0.4997	0.4998
3.5	0.4998	0.4998	0.4998	0.4998	0.4998	0.4998	0.4998	0.4998	0.4998	0.4998
3.6	0.4998	0.4998	0.4999	0.4999	0.4999	0.4999	0.4999	0.4999	0.4999	0.4999
3.7	0.4999	0.4999	0.4999	0.4999	0.4999	0.4999	0.4999	0.4999	0.4999	0.4999
3.8	0.4999	0.4999	0.4999	0.4999	0.4999	0.4999	0.4999	0.4999	0.4999	0.4999
3.9	0.5000	0.5000	0.5000	0.5000	0.5000	0.5000	0.5000	0.5000	0.5000	0.5000

APPENDIX C2. PERCENTILES OF *t*-DISTRIBUTION

Significant level (α) 2-sided confidence level 1-sided confidence level	0.8 20 60	0.6 40 70	0.4 60 80	0.2 80 90	0.1 90 95	0.05 95 97.5	0.02 98 99	0.01 99 99.5
1	0.325	0.727	1.376	3.078	6.314	12.706	31.821	63.657
2	0.289	0.617	1.061	1.886	2.920	4.303	6.965	9.925
3	0.277	0.584	0.978	1.638	2.353	3.182	4.541	5.841
4	0.271	0.569	0.941	1.533	2.132	2.776	3.747	4.604
5	0.267	0.559	0.920	1.476	2.015	2.571	3.365	4.032
6	0.265	0.553	0.906	1.440	1.943	2.447	3.143	3.707
7	0.263	0.549	0.896	1.415	1.895	2.365	2.998	3.499
8	0.262	0.546	0.889	1.397	1.860	2.306	2.896	3.355
9	0.261	0.543	0.883	1.383	1.833	2.262	2.821	3.250
10	0.260	0.542	0.879	1.372	1.812	2.228	2.764	3.169
11	0.260	0.540	0.876	1.363	1.796	2.201	2.718	3.106
12	0.259	0.539	0.873	1.356	1.782	2.179	2.681	3.055
13	0.259	0.538	0.870	1.350	1.771	2.160	2.650	3.012
14	0.258	0.537	0.868	1.345	1.761	2.145	2.624	2.977
15	0.258	0.536	0.866	1.341	1.753	2.131	2.602	2.947
16	0.258	0.535	0.865	1.337	1.746	2.120	2.583	2.921
17	0.257	0.534	0.863	1.333	1.740	2.110	2.567	2.898
18	0.257	0.534	0.862	1.330	1.734	2.101	2.552	2.878
19	0.257	0.533	0.861	1.328	1.729	2.093	2.539	2.861
20	0.257	0.533	0.860	1.325	1.725	2.086	2.528	2.845
21	0.257	0.532	0.859	1.323	1.721	2.080	2.518	2.831
22	0.256	0.532	0.858	1.321	1.717	2.074	2.508	2.819
23	0.256	0.532	0.858	1.319	1.714	2.069	2.500	2.807
24	0.256	0.531	0.857	1.318	1.711	2.064	2.492	2.797
25	0.256	0.531	0.856	1.316	1.708	2.060	2.485	2.787
26	0.256	0.531	0.856	1.315	1.706	2.056	2.479	2.779
27	0.256	0.531	0.855	1.314	1.703	2.052	2.473	2.771
28	0.256	0.530	0.855	1.313	1.701	2.048	2.467	2.763
29	0.256	0.530	0.854	1.311	1.699	2.045	2.462	2.756
30	0.256	0.530	0.854	1.310	1.697	2.042	2.457	2.750
40	0.255	0.529	0.851	1.303	1.684	2.021	2.423	2.704
50	0.255	0.528	0.849	1.299	1.676	2.009	2.403	2.678
60	0.254	0.527	0.848	1.296	1.671	2.000	2.390	2.660
120	0.254	0.526	0.845	1.289	1.658	1.980	2.358	2.617
∞	0.253	0.524	0.842	1.282	1.645	1.960	2.327	2.576